## University of Mumbai

## Examination 2021 under Cluster 06

(Lead College: Vidyavardhini's College of Engg Tech)
Examination for Direct Second Year Students Commencing from 10 ${ }^{\text {th }}$ April 2021
Program: Electronics Engineering
Curriculum Scheme: Rev 2019
Examination: SE Semester III (For DSE Students)
Course Code: ELC304 and Course Name: Electrical Network Analysis and Synthesis
Time: 2 hour
Max. Marks: 80

| Q1. | Choose the correct option for following questions. All the Questions are compulsory and carry equal marks |
| :---: | :---: |
| 1. | $\qquad$ between coils is defined as fraction of magnetic flux produced by the current in one coil that links the other |
| Option A: | Coefficient of Coupling |
| Option B: | Self Inductance |
| Option C: | Mutual Inductance |
| Option D: | Self Coupling |
| 2. | The combined inductance of two coils connected in series is 0.6 H or 0.1 H depending on relative directions of currents in the two coils. If one of the coils has a self-inductance of 0.2 H , find (a) mutual inductance, and (b) coefficient of coupling. |
| Option A: | (a)M $=0.105 \mathrm{H}$, (b) $\mathrm{K}=0.62$ |
| Option B: | (a)M $=0.125 \mathrm{H}$, (b) $\mathrm{K}=0.72$ |
| Option C: | (a)M=0.115H, (b) $\mathrm{K}=0.72$ |
| Option D: | (a)M $\mathrm{M}=0.125 \mathrm{H}$, (b) $\mathrm{K}=0.62$ |
| 3. | Which notation of instant implies that the unchanged condition of network is about to change? |
| Option A: | $\mathrm{t}(0)^{+}$ |
| Option B: | t(0)- |
| Option C: | $t^{*}$ |
| Option D: | t |
| 4. | What does ' $\sigma$ ' indicate in the equation of complex frequency variable $s=\sigma+j \omega$ while defining the Laplace transform? |
| Option A: | Attenuation constant |
| Option B: | Damping factor |


| Option C: | Propagation constant |
| :---: | :---: |
| Option D: | Phase constant |
| 5. | Consider a function $\mathrm{f}(\mathrm{t})$ that satisfies the differential equation given below. What equation will be generated by taking Laplace transform and replacing the terms $\mathrm{f}\left(0^{-}\right) \& \mathrm{f}^{\prime}\left(0^{-}\right)$by zero? <br> $\left[\mathrm{d}^{2} \mathrm{f}(\mathrm{t}) / \mathrm{dt}^{2}\right]+5[\mathrm{df}(\mathrm{t}) / \mathrm{dt}]+6 \mathrm{f}(\mathrm{t})=10$ |
| Option A: | $\left[\mathrm{S}^{2} \mathrm{~F}(\mathrm{~s})+5 \mathrm{~s} \mathrm{~F}(\mathrm{~s})+6 \mathrm{~F}(\mathrm{~s})\right]=10 / \mathrm{s}$ |
| Option B: | $\left[\mathrm{S}^{2} \mathrm{~F}(\mathrm{~s})+5 \mathrm{sF}(\mathrm{s})-6 \mathrm{~F}(\mathrm{~s})\right]=10 / \mathrm{s}$ |
| Option C: | $\left[\mathrm{S}^{2} \mathrm{~F}(\mathrm{~s})-5 \mathrm{sF}(\mathrm{s})+6 \mathrm{~F}(\mathrm{~s})\right]=10 / \mathrm{s}$ |
| Option D: | $\left[\mathrm{S}^{2} \mathrm{~F}(\mathrm{~s})-5 \mathrm{sF}(\mathrm{s})-6 \mathrm{~F}(\mathrm{~s})\right]=10 / \mathrm{s}$ |
| 6. | What is an ideal value of network function at poles? |
| Option A: | Zero |
| Option B: | Nonzero |
| Option C: | Infinity |
| Option D: | Unity |
| 7. | The realization of driving point immitance functions of networks can be done by any of the forms which are not used from following |
| Option A: | Foster I |
| Option B: | Foster II |
| Option C: | Cauer I |
| Option D: | Curier II |
| 8. | Which among the following represents the precise condition of reciprocity for transmission parameters? |
| Option A: | AD-BC=0 |
| Option B: | $\mathrm{AC}-\mathrm{BD}=1$ |
| Option C: | $\mathrm{AD}-\mathrm{BC}=1$ |
| Option D: | $\mathrm{BC}-\mathrm{AD}=1$ |
| 9. | The relation between $\mathrm{Z}_{\mathrm{OT}}, \mathrm{Z}_{\mathrm{oc}}, \mathrm{Z}_{\mathrm{sc}}$ is? |
| Option A: | $\mathrm{Z}_{\mathrm{OT}}=\sqrt{ } \mathrm{Z}_{\mathrm{oc}} \mathrm{Z}_{\mathrm{sc}}$ |
| Option B: | $\left.\mathrm{Z}_{\mathrm{oc}}=\sqrt{( } \mathrm{Z}_{\mathrm{OT}} \mathrm{Z}_{\mathrm{sc}}\right)$ |
| Option C: | $\mathrm{Z}_{\mathrm{sc}}=\sqrt{ }\left(\mathrm{Z}_{\mathrm{OT}} \mathrm{Z}_{\mathrm{oc}}\right)$ |
| Option D: | $\mathrm{Z}_{\mathrm{oc}}=\sqrt{ }\left(\mathrm{Z}_{\mathrm{OT}} \mathrm{Z}_{\mathrm{oc}}\right)$ |
| 10. | In determining Hybrid parameters, among $\mathrm{V}_{1}, \mathrm{~V}_{2}, \mathrm{I}_{1}, \mathrm{I}_{2}$, which of the following |


|  | are dependent variables? |
| :---: | :---: |
| Option A: | $\mathrm{V}_{1}$ and $\mathrm{V}_{2}$ |
| Option B: | $\mathrm{I}_{1}$ and $\mathrm{I}_{2}$ |
| Option C: | $\mathrm{V}_{1}$ and $\mathrm{I}_{2}$ |
| Option D: | $\mathrm{I}_{1}$ and $\mathrm{V}_{2}$ |
| 11. | The Laplace transform of a unit-ramp function starting at $\mathrm{t}=\mathrm{a}$ is |
| Option A: | $\frac{1}{(s+a)^{2}}$ |
| Option B: | $\frac{e^{-a s}}{(s+a)^{2}}$ |
| Option C: | $\frac{e^{-a s}}{s^{2}}$ |
| Option D: | $\frac{a}{s^{2}}$ |
| 12. |  <br> Fig. 7.4 <br> Above pole zero diagram indicates which function |
| Option A: | RC |
| Option B: | LC |
| Option C: | RL |
| Option D: | RLC |
| 13. | A system is represented by the transfer function $10 /(\mathrm{S}+2)(\mathrm{s}+1)$, The dc gain of this system is |
| Option A: | 1 |
| Option B: | 5 |
| Option C: | 10 |
| Option D: | 2 |
|  |  |
| 14. | The transfer function of a low-pass RC network is |


| Option A: | $(R C s)(1+R C s)$ |
| :---: | :---: |
| Option B: | $\frac{R C s}{1+R C s}$ |
| Option C: | $\frac{1}{1+R C s}$ |
| Option D: | $\frac{s}{1+R C s}$ |
| 15. | The input ports of two networks are connected in series and the output ports are connected in parallel ,then resultant h-parameter matrix is the ---------- of h-parameter matrices of each individual two-port network |
| Option A: | Substraction |
| Option B: | Division |
| Option C: | Multiplication |
| Option D: | Sum |
| 16. | For a two-port network to be reciprocal |
| Option A: | $\mathrm{z} 11=\mathrm{z} 22$ |
| Option B: | $\mathrm{y} 21=\mathrm{y} 12$ |
| Option C: | $\mathrm{h} 21=\mathrm{h} 12$ |
| Option D: | $\mathrm{AD}-\mathrm{BC}=0$ |
| 17. | The number of roots of $\mathrm{s}^{3}+5 \mathrm{~s}^{2}+7 \mathrm{~s}+3=0$ in the right half of s-plane is |
| Option A: | Zero |
| Option B: | One |
| Option C: | Two |
| Option D: | Three |
| 18. | The circuit shown in Fig. is |
| Option A: | Cauer I form |
| Option B: | Cauer II form |
| Option C: | Foster I form |
| Option D: | Foster II form |
| 19. | From below functions which is positive real function |
| Option A: | $F(s)=\frac{s^{3}+5 s}{s^{4}+2 s^{2}+1}$ |
| Option B: | $F(s)=\frac{s^{2}+s+6}{s^{2}+s+1}$ |


| Option C: | $F(s)=\frac{s^{2}+4}{s^{3}+3 s^{2}+3 s+1}$ |
| :---: | :--- |
| Option D: | $F(s)=\frac{s^{3}+6 s^{2}+7 s+3}{s^{2}+2 s+1}$ |
| 20. | Find the nominal impedance, cut-off frequency for the network shown in fig. |
|  |  |


| Q2 |
| :---: | :--- | :--- |
| $\mathbf{( 2 0 ~ M a r k s ) ~}$ | Solve any Four out of Six (5 marks each)



| Q3 <br> (20 Marks) |  |
| :---: | :--- |
| Q.3 A | Solve any Two (5 marks each) |
| i. | Write short note on Different types of filter |
| ii. | Determine the transmission parameters for the network shown in Fig. |
|  |  |
| iii. | Solve any One (10 marks each) |
| i. | a) Prove that polynomial $P(s)=s^{4}+s^{3}+2 s^{2}+3 s+2$ is not Hurwitz. |


|  | b) Test whether the polynomial $\mathrm{P}(\mathrm{s})=\mathrm{s}^{8}+5 \mathrm{~s}^{6}+2 \mathrm{~s}^{4}+3 \mathrm{~s}^{2}+1$ is Hurwitz by <br> Routh array |
| :---: | :--- |
| ii. | Realise Foster I \& Cauer I forms of the following RC impedance function <br> $Z(s)=\frac{s+4}{(s+2)(s+6)}$ |

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Max. Marks: 80
Q1:

| Question <br> Number | Correct Option <br> (Enter either 'A' or 'B' <br> or ' $\mathbf{C}^{\prime}$ or ' $\mathbf{D}$ ') |
| :---: | :---: |
| Q1. | A |
| Q2. | B |
| Q3. | B |
| Q4 | A |
| Q5 | A |
| Q6 | C |
| Q7 | D |
| Q8. | C |
| Q9. | A |
| Q10. | C |
| Q11. | C |
| Q12. | B |
| Q13. | B |
| Q14. | C |
| Q15. | D |
| Q16. | B |
| Q17. | A |
| Q18. | C |
| Q19. | D |
| Q20. | A |
|  |  |

Important steps and final answer for the questions involving numerical example Q2(A):

Solution The equivalent circuit in terms of dependent sources is shown in Fig. 4.52.


Q2(B):

Solution The current $\mathbf{I}_{1}$ leaves from the dotted end and $\mathbf{I}$, enters from the dotted end. Hence, mutual inductance $M$ is negative
In the conductively coupled equivalent circuit,
$\mathbf{Z}_{1}=j \omega\left(L_{1}-M\right)=j \omega L_{1}-j \omega M=j 3-j 2=j 1 \Omega$
$\mathbf{Z}_{2}=j \omega\left(L_{2}-M\right)=j \omega L_{2}-j \omega M=j 5-j 2=j 3 \Omega$
$\mathbf{Z}_{3}=j \omega M=j 2 \Omega$
The conductively coupled equivalent circuit is shown in Fig. 4.76.


Q2(C):
Solution At $t=0$, the network attains steady-state condition. Hence, the capacitor acts as an open circuit.

$$
v_{C}\left(0^{-}\right)=30 \mathrm{~V}
$$

$$
i\left(0^{-}\right)=0
$$

At $t=0^{+}$, the network is shown in Fig. 6.27.
At $t=0^{+}$, the capacitor acts as a voltage source of 30 v

$$
\begin{aligned}
v_{C}\left(0^{+}\right) & =30 \mathrm{~V} \\
i\left(0^{+}\right) & =-\frac{30}{30}=-1 \mathrm{~A}
\end{aligned}
$$

For $t>0$, the network is shown in Fig. 6.28 .
$-10 i-20 i-\frac{1}{1 \times 10^{-6}} \int_{0}^{t} i d t-30=0$
...(i)
$-30 \frac{d i}{d t}-10^{6} i=0 \quad$...(ii)
At $t=0^{*}, \quad-30 \frac{d i}{d t}\left(0^{+}\right)-10^{6} i\left(0^{+}\right)=0$ $\frac{d i}{d t}\left(0^{+}\right)=\frac{10^{6}(-1)}{30}=0.33 \times 10^{5} \mathrm{~A} / \mathrm{s}$
At $t=0^{+}$,

$$
\begin{aligned}
& -30 \frac{d i}{d t}\left(0^{+}\right)-\frac{d^{2} i}{d t^{2}}\left(0^{+}\right)=0 \\
& \frac{d^{2} i}{d t^{2}}\left(0^{+}\right)=1800 \mathrm{~A} / \mathrm{s}^{2}
\end{aligned}
$$

Q2(D):
Solution At $t=0$, the capacitor is uncharged. Hence, it acts as a short circuit
$v_{C}\left(0^{-}\right)=0$
$i_{c}\left(0^{-}\right)=0$
At $t=0^{+}$, the network is shown in Fig. 6.130.
Since voltage across the capacitor cannot change
instantaneously,

$i_{C}\left(0^{+}\right)=1.02 \mathrm{~m} \times \frac{1 \mathrm{k}}{1 \mathrm{k}+4 \mathrm{k}}=0.204 \mathrm{~mA}$
For $t>0$, Thevenin's equivalent network is shown in Fig. 6.132.
Writing the KCL equation for $t>0$.
Writing we KcL

$$
\begin{aligned}
3 \times 10^{-6} \frac{d v_{C}}{d t}+\frac{v_{C}-1}{4.9 \times 10^{3}} & =0 \\
\frac{d v_{C}}{d t}+68.02 v_{C} & =68.02
\end{aligned}
$$


Fig. 6.131

Fig. 6.132

Q2(E)
Solution At $t=0^{-}$, the network is shown in Fig 7.54. At
$t=0^{-}$, the switch is closed and steady-state condition is achieved $=0$, the switch is closed and steady-state condition is achieved.
Hence, the capacitor acts as an open circuit and the in Hence, the capacitor acts as an open circuit and the inductor acts a ( $(0)=1 \mathrm{~V}$ $i\left(0^{-}\right)=1$
Since current through the inductor and voltage across the
capacitor cannot change instantaneously,
$i\left(0^{\circ}\right)=1 \mathrm{~A}$


For $t>0$, the transformed network is shown in Fig 7.55
For $r>0$, KVL to the mesh for $t>0$,
$\frac{1}{s}-\frac{1}{s} I(s)-0.5 s I(s)+0.5-I(s)=0$

$$
0.5+\frac{1}{s}=\frac{1}{s} I(s)+0.5 s I(s)+I(s)
$$

$I(s)\left[1+\frac{1}{s}+0.5 s\right]=0.5+\frac{1}{s}$
$I(s)=\frac{s+2}{s^{2}+2 s+2}=\frac{(s+1)+1}{(s+1)^{2}+1}=\frac{s+1}{(s+1)^{2}+1}+\frac{1}{(s+1)^{2}+1}$
Taking the inverse Laplace transform,

$$
i(t)=e^{-t} \cos t+e^{-t} \sin t \quad \text { for } t>0
$$



Fig. 7.54
$i(t)=e^{-t} \cos t+e^{-t} \sin t$

Substituting Eq. (ii) in Eq. (i),

$$
\begin{aligned}
I_{1} & =\frac{s+1}{s}\left[(s+1) V_{2}-I_{2}\right]-V_{2} \\
& =\left[\frac{(s+1)^{2}}{s}-1\right] V_{2}-\frac{s+1}{s} I_{2} \\
& =\left(\frac{s^{2}+s+1}{s}\right) V_{2}-\left(\frac{s+1}{s}\right) I_{2}
\end{aligned}
$$

Comparing Eqs (ii) and (iii) with $A B C D$ parameter equations,

$$
\left[\begin{array}{ll}A & B \\ C & D\end{array}\right]=\left[\begin{array}{cc}s+1 & 1 \\ \frac{s^{2}+s+1}{s} & \frac{s+1}{s}\end{array}\right]
$$

## Q3(A3):



## Q3(B1-a):

Solution Even part of $P(s)=m(s)=s^{4}+2 s^{2}+2$
Odd part of $P(s)=n(s)=s^{3}+3 s$

$$
Q(s)-\frac{m(s)}{n(s)}
$$

By continued fraction expansion,

$$
\begin{aligned}
& \left.s^{3}+3 s\right) s^{4}+2 s^{2}+2(s \\
& \frac{s^{4}+3 s^{2}}{\left.-s^{2}+2\right) s^{3}+3 s(-s}
\end{aligned}
$$

$$
s^{3}-2 s
$$

$$
5 s)-s^{2}+2\left(-\frac{1}{5} s\right.
$$

$$
-s^{2}
$$

$$
2 \cdot) \cdot\left(\frac{s}{2}\right.
$$

$$
\frac{5 s}{0}
$$

Since two quotient terms are negative, $P(s)$ is not Hurwitz.
Q3(B1-b):

Solution The given polynomial contains even functions only.
The Routh array is given by,

| $s^{8}$ | 1 | 5 | 2 | 3 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $s^{7}$ | 8 | 30 | 8 | 6 | 0 |
| $s^{6}$ | 1.25 | 1 | 2.25 | 1 |  |
| $s^{5}$ | 23.6 | -6.4 | -0.4 | 0 |  |
| $s^{4}$ | 1.33 | 2.27 | 1 |  |  |
| $s^{3}$ | -46.6 | -18.14 | 0 |  |  |
| $s^{2}$ | 1.75 | 1 |  |  |  |
| $s^{1}$ | 8.49 |  |  |  |  |
| $s^{0}$ | 1 |  |  |  |  |

Since there is a sign change in the first column of the array, the polynomial is not Hurwitz
Q3(B2):

## Solution

Caver I Form The Cauer I form is obtained by continued fraction expansion of $Z(s)$ about the pole at
infinity. In the above function, the degree of the numerator is less than the degree of the denominator which
indicates presence of a zero at infinity. Hence, the admittance function $Y(s)$ has a pole at infinity
By continued fraction expansion, $\quad Y(s)=\frac{{ }^{2}+8}{s+4}$
By
$s+4) s^{2}+8 s+12(s \leftarrow Y$
 admittances are connected in parallel branches. The network is show in Fig. 10.55.
Foster I Form The Foster I form is obtained by partial fraction

$$
Z(s)=\frac{s+4}{(s+2)(s+6)}
$$

$$
Z(s)=\frac{s+4}{(s+2)(s+6)}
$$

Fig. 10.56
By partial-fraction expansion,

$$
Z(s)=\frac{K_{1}}{s+2}+\frac{K_{2}}{s+6}
$$

where $\quad K_{1}=\left.(s+2) Z(s)\right|_{s=-2}=\frac{(-2+4)}{(-2+6)}=\frac{1}{2}$

$$
K_{2}=\left.(s+6) Z(s)\right|_{s=-6}=\frac{(-6+4)}{(-6+2)}=\frac{1}{2}
$$

$$
Z(s)=\frac{\frac{1}{2}}{s+2}+\frac{\frac{1}{2}}{s+6}
$$

$$
\begin{aligned}
& \text { These two terms represent the impedance of a parallel } R C \text { circuit for which } \\
& \text { Ther }
\end{aligned}
$$

$$
Z_{R C}(s)=\frac{\frac{1}{C_{i}}}{s+\frac{1}{R_{i} C_{i}}}
$$

By direct comparison,

$$
\begin{array}{ll}
R_{1}=\frac{1}{4} \Omega, & C_{1}=2 \mathrm{~F} \\
R_{2}=\frac{1}{12} \Omega, & C_{2}=2 \mathrm{~F}
\end{array}
$$


10.56.

